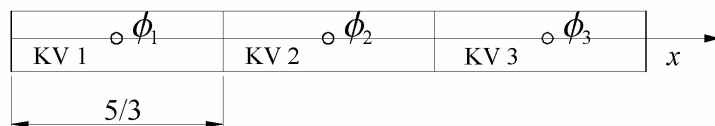


RJEŠENJA 2. KOLOKVIJA NUMERICKE METODE U STROJARSTVU

1. Potrebno je izvesti sustav jednažbi za rješavanje jednodimenzijske Poissonove diferencijalne jednažbe $5 \frac{d^2\phi}{dx^2} = 10x$ zadane na području $0 \leq x \leq 5$. Problem diskretizirati s tri volumena.

Zadani rubni uvjeti: $\phi(5) = 40, 5 \frac{d\phi}{dx}(0) = 100$.

Proračunski model:



Integrirajući jednažbu $5 \frac{d^2\phi}{dx^2} = 10x$ po konačnom volumenu dobivamo

$$\int_V 5 \frac{d}{dx} \left(\frac{d\phi}{dx} \right) dV = \int_V 10x dV$$

$$\int_V 5 \frac{d}{dx} \left(\frac{d\phi}{dx} \right) dV = 5 \int_S \left(\frac{d\phi}{dx} \right) n_x dS$$

$$5 \int_S \left(\frac{d\phi}{dx} \right) n_x dS = 5 \sum_c \int_{S_c} \left(\frac{d\phi}{dx} \right) n_x^c dS_c$$

$$5 \sum_c \int_{S_c} \left(\frac{d\phi}{dx} \right) n_x^c dS_c = 5 \sum_c \left(\frac{d\phi}{dx} \right)_c n_x^c \Delta S_c$$

$$5 \sum_c \left(\frac{d\phi}{dx} \right)_c n_x^c \Delta S_c = 10x_p \Delta V$$

$c = e, w$ su sredine stranice volumena, n_x^c komponenta normale po osi x na sredini stranice c , ΔS_c ploština stranice c , x_p koordinata središta volumena, ΔV veličina volumena.

$$5 \left\{ \left(\frac{d\phi}{dx} \right)_e - \left(\frac{d\phi}{dx} \right)_w \right\} = 10x_p \Delta x$$

KV 1:

$$\left(\frac{d\phi}{dx} \right)_e \approx \frac{\phi_2 - \phi_1}{5/3}; 5 \left(\frac{d\phi}{dx} \right)_w = 100 \rightarrow \left\{ 5 \frac{\phi_2 - \phi_1}{5/3} - 100 \right\} = 10 \frac{5}{6} \frac{5}{3}$$

$$-3\phi_1 + 3\phi_2 = \frac{2050}{18}$$

KV 2:

$$\left(\frac{d\phi}{dx} \right)_e \approx \frac{\phi_3 - \phi_2}{5/3}; \left(\frac{d\phi}{dx} \right)_w \approx \frac{\phi_2 - \phi_1}{5/3} \rightarrow 5 \left\{ \frac{\phi_3 - \phi_2}{5/3} - \frac{\phi_2 - \phi_1}{5/3} \right\} = 10 \frac{5}{2} \frac{5}{3}$$

$$3\phi_1 - 6\phi_2 + 3\phi_3 = \frac{750}{18}$$

KV 3:

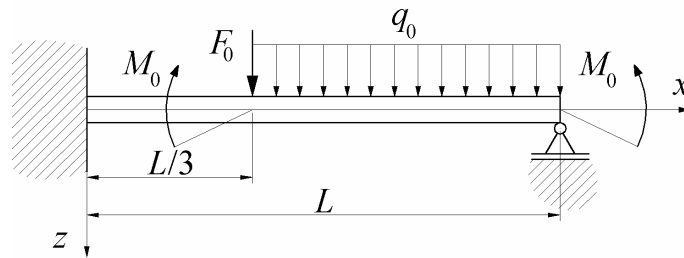
$$\left(\frac{d\phi}{dx} \right)_e \approx \frac{\phi_e^0 - \phi_3}{5/6}; \left(\frac{d\phi}{dx} \right)_w \approx \frac{\phi_3 - \phi_2}{5/3} \rightarrow 5 \left\{ \frac{40 - \phi_3}{5/6} - \frac{\phi_3 - \phi_2}{5/3} \right\} = 10 \frac{25}{6} \frac{5}{3}$$

$$3\phi_2 - 9\phi_3 = \frac{-3070}{18}$$

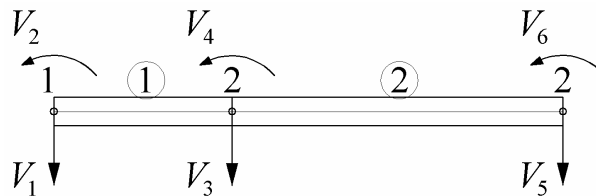
$$\begin{bmatrix} -3 & 3 & 0 \\ 3 & -6 & 3 \\ 0 & 3 & -9 \end{bmatrix} \begin{bmatrix} \phi_1 \\ \phi_2 \\ \phi_3 \end{bmatrix} = \frac{1}{18} \begin{bmatrix} 2050 \\ 750 \\ -3070 \end{bmatrix}.$$

3. Za nosač zadan i opterećen prema slici potrebno je odrediti vektor čvornih opterećenja prikazan u globalnim stupnjevima slobode pomoću metode konačnih elemenata. Problem diskretizirati s dva osnovna gredna elementa. Prikazati izračunavanje raspodjele momenta savijanja za element koji uključuje uklještenje, bez izračunavanja stupnjeva slobode.

Zadano: $L, q_0, F_0 = q_0L, M_0 = q_0L^2, EI = \text{konst.}$



$$\mathbf{N} = \left[\left(1 - \frac{3x^2}{l^2} + \frac{2x^3}{l^3} \right) \quad \left(-x + \frac{2x^2}{l} - \frac{x^3}{l^2} \right) \quad \left(\frac{3x^2}{l^2} - \frac{2x^3}{l^3} \right) \quad \left(\frac{x^2}{l} - \frac{x^3}{l^2} \right) \right], \quad \mathbf{F}_s^T = q_0L \begin{bmatrix} \frac{1}{3} & -\frac{L}{27} & \frac{1}{3} & \frac{L}{27} \end{bmatrix}.$$



$$\mathbf{V}^T = [V_1 \quad V_2 \quad V_3 \quad V_4 \quad V_5 \quad V_6].$$

$$\mathbf{R}^T = [R_1 \quad R_2 \quad R_3 \quad R_4 \quad R_5 \quad R_6].$$

$$(\mathbf{F}_s^2)^T = q_0L \begin{bmatrix} \frac{1}{3} & -\frac{L}{27} & \frac{1}{3} & \frac{L}{27} \end{bmatrix}.$$

$$(\mathbf{R}_s^2)^T = q_0L \begin{bmatrix} 0 & 0 & \frac{1}{3} & -\frac{L}{27} & \frac{1}{3} & \frac{L}{27} \end{bmatrix}.$$

$$(\mathbf{F})^T = q_0L [0 \quad 0 \quad 1 \quad -L \quad 0 \quad L].$$

$$(\mathbf{R})^T = q_0L \begin{bmatrix} 0 & 0 & \frac{1}{3} + 1 & -\frac{L}{27} - L & \frac{1}{3} & \frac{L}{27} + L \end{bmatrix} = q_0L \begin{bmatrix} 0 & 0 & \frac{4}{3} & -\frac{28L}{27} & \frac{1}{3} & \frac{28L}{27} \end{bmatrix}.$$

Raspodjela momenta savijanja po elementu 1:

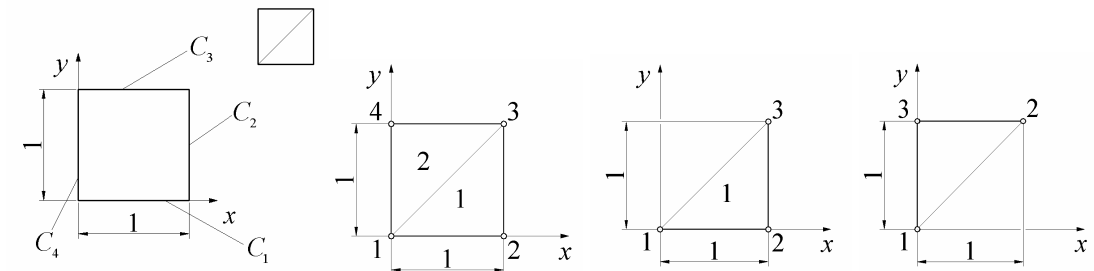
$$M_y^1 = -EI \frac{d^2 w^1}{dx^2} = -EI \begin{bmatrix} \frac{d^2 N_1}{dx^2} & \frac{d^2 N_2}{dx^2} & \frac{d^2 N_3}{dx^2} & \frac{d^2 N_4}{dx^2} \end{bmatrix} \begin{bmatrix} v_1^1 \\ v_2^1 \\ v_3^1 \\ v_4^1 \end{bmatrix}.$$

$$M_y^1 = -EI \begin{bmatrix} \left(\frac{-6}{l^2} + \frac{12x}{l^3} \right) & \left(\frac{4}{l} - \frac{6x}{l^2} \right) & \left(\frac{6}{l^2} - \frac{12x}{l^3} \right) & \left(\frac{2}{l} - \frac{6x}{l^2} \right) \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ V_3 \\ V_4 \end{bmatrix}.$$

4. Zadan je problem provođenja topline s konstantnim toplinskim izvorom q . Za diskretizaciju s dva trokutna elementa prema slici izračunati temperature u čvorovima. Za prikazane konačne elemente matrice krutosti su

$$\mathbf{k}^1 = \frac{1}{2} \begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix}, \quad \mathbf{k}^2 = \frac{1}{2} \begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & -1 \\ -1 & -1 & 2 \end{bmatrix}. \quad \text{Zadano: } \rho = 1 \text{ kg/m}^3, \lambda = 16 \text{ W/mK}, q = 1 \text{ W/kg}.$$

Rubni uvjeti su: $C_1: \lambda \frac{\partial T}{\partial y} = 0$; $C_2: \lambda \frac{\partial T}{\partial x} = 96$; $C_3: T = 3x^2 + 5$; $C_4: \lambda \frac{\partial T}{\partial x} = 0$.



$$\mathbf{k} = \frac{1}{4A} \begin{bmatrix} \beta_1^2 + \gamma_1^2 & \beta_1\beta_2 + \gamma_1\gamma_2 & \beta_1\beta_3 + \gamma_1\gamma_3 \\ \beta_2\beta_1 + \gamma_2\gamma_1 & \beta_2^2 + \gamma_2^2 & \beta_2\beta_3 + \gamma_2\gamma_3 \\ \beta_3\beta_1 + \gamma_3\gamma_1 & \beta_3\beta_2 + \gamma_3\gamma_2 & \beta_3^2 + \gamma_3^2 \end{bmatrix}, \quad \int_A N_i^i N_j^j N_k^k dA = \frac{i!j!k!}{(i+j+k+2)!} 2A$$

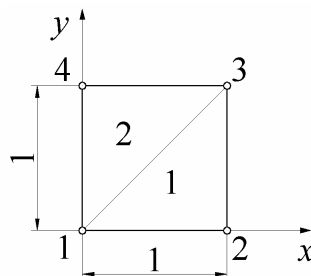
$$\alpha_1 = x_2 y_3 - x_3 y_2, \quad \beta_1 = y_2 - y_3, \quad \gamma_1 = x_3 - x_2,$$

$$\alpha_2 = x_3 y_1 - x_1 y_3, \quad \beta_2 = y_3 - y_1, \quad \gamma_2 = x_1 - x_3, \quad N_i = \frac{1}{2A} (\alpha_i + x\beta_i + y\gamma_i), \quad i = 1, 2, 3.$$

$$\alpha_3 = x_1 y_2 - x_2 y_1, \quad \beta_3 = y_1 - y_2, \quad \gamma_3 = x_2 - x_1$$

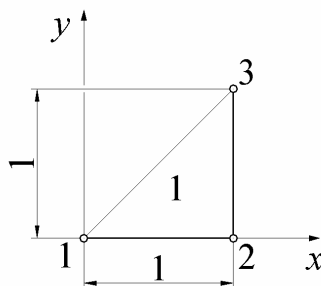
$$-\frac{\partial^2 T}{\partial x_i \partial x_i} = \frac{\rho q}{\lambda}$$

Proračunski model:



$$\mathbf{T}^T = [T_1 \quad T_2 \quad T_3 \quad T_4].$$

KE 1:

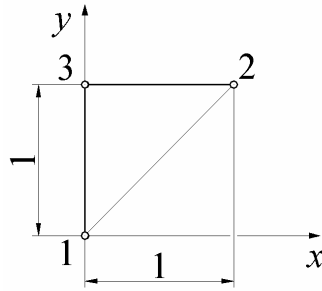


$$\beta_1 = -1, \quad \gamma_1 = 0,$$

$$\beta_2 = 1, \quad \gamma_2 = -1,$$

$$\beta_3 = 0, \quad \gamma_3 = 1$$

$$\mathbf{k}^1 = \frac{1}{4 \cdot 0,5} \begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix}.$$



$$\beta_1 = 0, \quad \gamma_1 = -1, \\ \beta_2 = 1, \quad \gamma_2 = 0, \quad \mathbf{k}^2 = \frac{1}{4 \cdot 0,5} \begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & -1 \\ -1 & -1 & 2 \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 1 & 0 & -1 \\ 0 & 1 & -1 \\ -1 & -1 & 2 \end{bmatrix}. \\ \beta_3 = -1, \quad \gamma_3 = 1$$

Globalne čvorne varijable		1	2	3	4
Elementi, lokalne čv. var.	1	1	2	3	-
	2	1	-	2	3

$$\mathbf{K}^1 = \frac{1}{2} \begin{bmatrix} 1 & -1 & 0 & 0 \\ -1 & 2 & -1 & 0 \\ 0 & -1 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}. \\ \mathbf{K}^2 = \frac{1}{2} \begin{bmatrix} 1 & 0 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}.$$

$$\mathbf{F}_S^1 = \int_A \mathbf{N}^T f \, dA = \int_A \begin{bmatrix} N_1 \\ N_2 \\ N_3 \end{bmatrix} \frac{\rho q}{\lambda} \, dA = \int_A N_1^i N_2^j N_3^k \, dA = \frac{i!j!k!}{(i+j+k+2)!} 2A.$$

$$\int_A N_1 \, dA = \frac{1!}{(1+2)!} 2 \cdot 0,5 = \frac{1}{6}.$$

$$\int_A N_2 \, dA = \frac{1!}{(1+2)!} 2 \cdot 0,5 = \frac{1}{6}.$$

$$\int_A N_3 \, dA = \frac{1!}{(1+2)!} 2 \cdot 0,5 = \frac{1}{6}.$$

$$\mathbf{F}_S^1 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}, \quad \mathbf{F}_S^2 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}.$$

$$\mathbf{R}_S^1 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 1 \\ 0 \end{bmatrix}, \quad \mathbf{R}_S^2 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}.$$

$$\mathbf{R}_S = \mathbf{R}_S^1 + \mathbf{R}_S^2 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 2 \\ 1 \\ 2 \\ 1 \end{bmatrix}.$$

$$\mathbf{K} = \mathbf{K}^1 + \mathbf{K}^2 = \frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & -1 \\ -1 & 2 & -1 & 0 \\ 0 & -1 & 2 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}.$$

Prirodni rubni uvjeti

$$C_2 : \mathbf{F}_b^1 = \int_l \mathbf{N}^T b_c dl.$$

$$\mathbf{F}_b^1 = \int_0^1 \begin{bmatrix} 0 \\ 1-y \\ y \end{bmatrix} 6 dy = \begin{bmatrix} 0 \\ 3 \\ 3 \end{bmatrix}.$$

$$\mathbf{R}_b^1 = \begin{bmatrix} 0 \\ 3 \\ 3 \\ 0 \end{bmatrix}.$$

$$\mathbf{R} = \mathbf{R}_s + \mathbf{R}_b^1 = \frac{1}{96} \begin{bmatrix} 2 \\ 1 \\ 2 \\ 1 \end{bmatrix} + \begin{bmatrix} 0 \\ 3 \\ 3 \\ 0 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2 \\ 289 \\ 290 \\ 1 \end{bmatrix}.$$

Osnovni rubni uvjeti

$$T_3 = 8, T_4 = 5.$$

$$\frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & -1 \\ -1 & 2 & -1 & 0 \\ 0 & -1 & 2 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2 \\ 289 \\ 290 \\ 1 \end{bmatrix},$$

$$\frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & -1 \\ -1 & 2 & 0 & 0 \\ 0 & 0 & 2 & 0 \\ -1 & 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2 \\ 289 \\ 290 \\ 1 \end{bmatrix} - 8 \frac{1}{2} \begin{bmatrix} 0 \\ -1 \\ 2 \\ -1 \end{bmatrix},$$

$$\frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & 0 \\ -1 & 2 & 0 & 0 \\ 0 & 0 & 2 & 0 \\ 0 & 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2 \\ 289 \\ 290 \\ 1 \end{bmatrix} - 8 \frac{1}{2} \begin{bmatrix} 0 \\ -1 \\ 2 \\ -1 \end{bmatrix} - 5 \frac{1}{2} \begin{bmatrix} -1 \\ 0 \\ 0 \\ 2 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2+240 \\ 289+384 \\ 290 \\ 1 \end{bmatrix}.$$

$$\frac{1}{2} \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 242 \\ 673 \end{bmatrix}.$$

$$\begin{bmatrix} T_1 \\ T_2 \end{bmatrix} = \begin{bmatrix} 8,0347 \\ 11,0278 \end{bmatrix}.$$