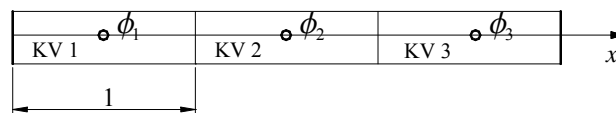


RJEŠENJA 2. KOLOKVIJA NUMERIČKE METODE U STROJARSTVU

1. . Potrebno je izvesti sustav jednadžbi za rješavanje jednodimenzijske Poissonove diferencijalne jednadžbe $\frac{d^2\phi}{dx^2} = -240x^2$ zadane na području $0 \leq x \leq 3$ pomoću metode konačnih volumena. Problem diskretizirati s tri volumena.

Zadani rubni uvjeti: $\phi(3) = -1600$, $\frac{d\phi}{dx}(0) = 7$.

Proračunski model:



Integrirajući jednadžbu $\frac{d^2\phi}{dx^2} = -240x^2$ po konačnom volumenu dobivamo

$$\begin{aligned} \int_V \frac{d^2\phi}{dx^2} dV &= \int_V -240x^2 dV, \\ \int_V \frac{d}{dx} \left(\frac{d\phi}{dx} \right) dV &= \int_V -240x^2 dV \\ \int_V \frac{d}{dx} \left(\frac{d\phi}{dx} \right) dV &= \int_S \left(\frac{d\phi}{dx} \right) n_x dS. \\ \iint_S \left(\frac{d\phi}{dx} \right) n_x dS &= \sum_c \int_{S_c} \left(\frac{d\phi}{dx} \right) n_x^c dS_c. \\ \sum_c \int_{S_c} \left(\frac{d\phi}{dx} \right) n_x^c dS_c &= \sum_c \left(\frac{d\phi}{dx} \right)_c n_x^c \Delta S_c. \\ \sum_c \left(\frac{d\phi}{dx} \right)_c n_x^c \Delta S_c &= -240(x_p)^2 \Delta V. \end{aligned}$$

$c = e, w$ su sredine stranica volumena, n_x^c komponenta normale po osi x na sredini stranice c , ΔS_c ploština stranice c , x_p koordinata središta volumena, ΔV veličina volumena.

$$\left\{ \left(\frac{d\phi}{dx} \right)_e - \left(\frac{d\phi}{dx} \right)_w \right\} = -240(x_p)^2 \Delta x.$$

KV 1:

$$\begin{aligned} \left(\frac{d\phi}{dx} \right)_e &\approx \frac{\phi_2 - \phi_1}{1}; \left(\frac{d\phi}{dx} \right)_w = 7 \rightarrow \{\phi_2 - \phi_1 - 7\} = -240(0,5)^2. \\ -\phi_1 + \phi_2 &= -53 \end{aligned}$$

KV 2:

$$\begin{aligned} \left(\frac{d\phi}{dx} \right)_e &\approx \frac{\phi_3 - \phi_2}{1}; \left(\frac{d\phi}{dx} \right)_w \approx \frac{\phi_2 - \phi_1}{1} \rightarrow \{\phi_3 - \phi_2 - (\phi_2 - \phi_1)\} = -240(1,5)^2. \\ \phi_1 - 2\phi_2 + \phi_3 &= -540 \end{aligned}$$

KV 3:

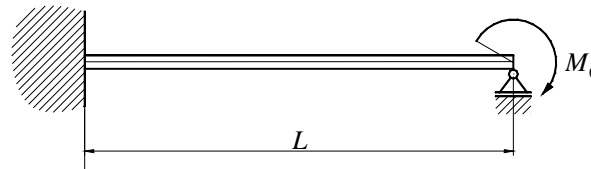
$$\left(\frac{d\phi}{dx} \right)_e \approx \frac{\phi_e^0 - \phi_3}{1/2}; \left(\frac{d\phi}{dx} \right)_w \approx \frac{\phi_3 - \phi_2}{1} \rightarrow \left\{ \frac{-1600 - \phi_3}{1/2} - (\phi_3 - \phi_2) \right\} = -240(2,5)^2.$$

$$\phi_2 - 3\phi_3 = 1700$$

$$\begin{bmatrix} -1 & 1 & 0 \\ 1 & -2 & 1 \\ 0 & 1 & -3 \end{bmatrix} \begin{bmatrix} \phi_1 \\ \phi_2 \\ \phi_3 \end{bmatrix} = \begin{bmatrix} -53 \\ -540 \\ 1700 \end{bmatrix}.$$

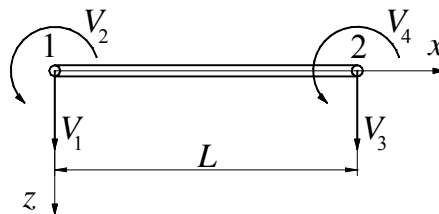
3. Za nosač zadan i opterećen prema slici potrebno je odrediti raspodjelu momenta savijanja pomoću metode konačnih elemenata. Problem diskretizirati osnovnim grednim elementom.

Zadano: $L, M_0, EI = \text{konst.}$



$$\mathbf{N} = \left[\left(1 - \frac{3x^2}{l^2} + \frac{2x^3}{l^3} \right) \quad \left(-x + \frac{2x^2}{l} - \frac{x^3}{l^2} \right) \quad \left(\frac{3x^2}{l^2} - \frac{2x^3}{l^3} \right) \quad \left(\frac{x^2}{l} - \frac{x^3}{l^2} \right) \right], \quad \mathbf{k} = EI \begin{bmatrix} \frac{12}{l^3} & -\frac{6}{l^2} & -\frac{12}{l^3} & -\frac{6}{l^2} \\ -\frac{6}{l^2} & \frac{4}{l} & \frac{6}{l^2} & \frac{2}{l} \\ -\frac{12}{l^3} & \frac{6}{l^2} & \frac{12}{l^3} & \frac{6}{l^2} \\ -\frac{6}{l^2} & \frac{2}{l} & \frac{6}{l^2} & \frac{4}{l} \end{bmatrix}.$$

Proračunski model



$$\mathbf{V}^T = [V_1 \quad V_2 \quad V_3 \quad V_4].$$

$$(\mathbf{R})^T = M_0 [0 \quad 0 \quad 0 \quad -1].$$

Jednadžba konačnog elementa

$$EI \begin{bmatrix} \frac{12}{L^3} & -\frac{6}{L^2} & -\frac{12}{L^3} & -\frac{6}{L^2} \\ -\frac{6}{L^2} & \frac{4}{L} & \frac{6}{L^2} & \frac{2}{L} \\ -\frac{12}{L^3} & \frac{6}{L^2} & \frac{12}{L^3} & \frac{6}{L^2} \\ -\frac{6}{L^2} & \frac{2}{L} & \frac{6}{L^2} & \frac{4}{L} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix} = M_0 \begin{bmatrix} 0 \\ 0 \\ 0 \\ -1 \end{bmatrix}$$

Rubni uvjeti pomaka:

$$V_1 = 0, V_2 = 0, V_3 = 0.$$

Nakon uvođenja rubnih uvjeta pomaka ostaje jednadžba

$$EI \frac{4}{L} V_4 = -M_0$$

$$V_4 = -\frac{M_0 L}{4EI}.$$

Raspodjela momenta savijanja po elementu 1:

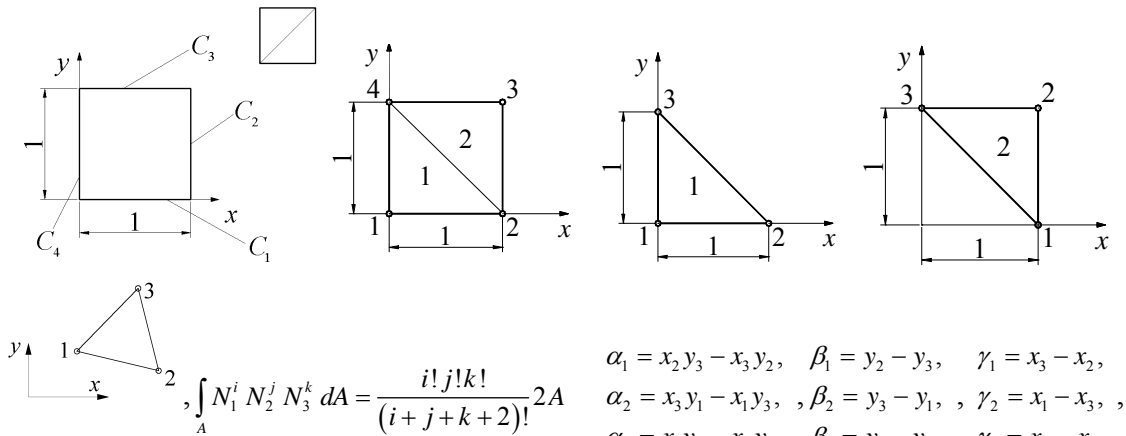
$$M_y = -EI \frac{d^2 w}{dx^2} = -EI \begin{bmatrix} \frac{d^2 N_1}{dx^2} & \frac{d^2 N_2}{dx^2} & \frac{d^2 N_3}{dx^2} & \frac{d^2 N_4}{dx^2} \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \end{bmatrix}$$

$$M_y = -EI \begin{bmatrix} \left(\frac{-6}{L^2} + \frac{12x}{L^3}\right) & \left(\frac{4}{L} - \frac{6x}{L^2}\right) & \left(\frac{6}{L^2} - \frac{12x}{L^3}\right) & \left(\frac{2}{L} - \frac{6x}{L^2}\right) \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ -\frac{M_0 L}{4EI} \end{bmatrix} = M_0 \left(\frac{1}{2} - \frac{3x}{2L}\right).$$

4. Zadan je problem provođenja topline s konstantnim toplinskim izvorom q . Za diskretizaciju s dva trokutna elementa prema slici izračunati temperaturu u sredini ploče. Za prikazane konačne elemente matrice koeficijenata su

$$\mathbf{k}^1 = \frac{1}{2} \begin{bmatrix} 2 & -1 & -1 \\ -1 & 1 & 0 \\ -1 & 0 & 1 \end{bmatrix}, \quad \mathbf{k}^2 = \frac{1}{2} \begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix}. \quad \text{Zadano: } \rho = 1 \text{ kg/m}^3, \alpha = 16 \text{ W/mK}, q = 1 \text{ W/kg}.$$

Rubni uvjeti su: $C_1 : \alpha \frac{\partial T}{\partial y} = 0$; $C_2 : \alpha \frac{\partial T}{\partial x} = 96$; $C_3 : T = 3x^2 + 5$; $C_4 : \alpha \frac{\partial T}{\partial x} = 0$.



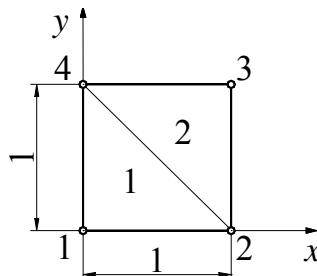
$$\int_A N_1^i N_2^j N_3^k dA = \frac{i!j!k!}{(i+j+k+2)!} 2A$$

$$\begin{aligned} \alpha_1 &= x_2 y_3 - x_3 y_2, & \beta_1 &= y_2 - y_3, & \gamma_1 &= x_3 - x_2, \\ \alpha_2 &= x_3 y_1 - x_1 y_3, & \beta_2 &= y_3 - y_1, & \gamma_2 &= x_1 - x_3, \\ \alpha_3 &= x_1 y_2 - x_2 y_1, & \beta_3 &= y_1 - y_2, & \gamma_3 &= x_2 - x_1 \end{aligned}$$

$$N_i = \frac{1}{2A} (\alpha_i + x\beta_i + y\gamma_i), \quad i = 1, 2, 3.$$

$$-\frac{\partial^2 T}{\partial x_i \partial x_i} = \frac{\rho q}{\alpha}.$$

Proračunski model:



$$\mathbf{T}^T = [T_1 \quad T_2 \quad T_3 \quad T_4].$$

Globalne čvorne varijable		1	2	3	4
Elementi, lokalne čv. var.	1	1	2	-	3
	2	-	1	2	3

$$\mathbf{K}^1 = \frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & -1 \\ -1 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 1 \end{bmatrix}.$$

$$\mathbf{K}^2 = \frac{1}{2} \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & -1 & 0 \\ 0 & -1 & 2 & -1 \\ 0 & 0 & -1 & 1 \end{bmatrix}.$$

$$\mathbf{F}_S^1 = \int_A \mathbf{N}^T f \, dA = \int_A \begin{bmatrix} N_1 \\ N_2 \\ N_3 \end{bmatrix} \frac{\rho q}{\lambda} \, dA = \int_A N_1^i N_2^j N_3^k \, dA = \frac{i!j!k!}{(i+j+k+2)!} 2A.$$

$$\int_A N_1 \, dA = \frac{1!}{(1+2)!} 2 \cdot 0.5 = \frac{1}{6}.$$

$$\int_A N_2 \, dA = \frac{1!}{(1+2)!} 2 \cdot 0.5 = \frac{1}{6}.$$

$$\int_A N_3 \, dA = \frac{1!}{(1+2)!} 2 \cdot 0.5 = \frac{1}{6}.$$

$$\mathbf{F}_S^1 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}, \quad \mathbf{F}_S^2 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}.$$

$$\mathbf{R}_S^1 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 1 \\ 0 \\ 1 \end{bmatrix}, \quad \mathbf{R}_S^2 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 0 \\ 1 \\ 1 \\ 1 \end{bmatrix}.$$

$$\mathbf{R}_S = \mathbf{R}_S^1 + \mathbf{R}_S^2 = \frac{1}{16} \frac{1}{6} \begin{bmatrix} 1 \\ 2 \\ 1 \\ 2 \end{bmatrix}.$$

$$\mathbf{K} = \mathbf{K}^1 + \mathbf{K}^2 = \frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & -1 \\ -1 & 2 & -1 & 0 \\ 0 & -1 & 2 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix}.$$

Prirodni rubni uvjeti

$$C_2 : \mathbf{F}_b^1 = \int_l \mathbf{N}^T b_c \, dl.$$

$$\mathbf{F}_b^2 = \int_0^1 \begin{bmatrix} 1-y \\ y \\ 0 \end{bmatrix} 6 \, dy = \begin{bmatrix} 3 \\ 3 \\ 0 \end{bmatrix}.$$

$$\mathbf{R}_b^2 = \begin{bmatrix} 0 \\ 3 \\ 3 \\ 0 \end{bmatrix}.$$

$$\mathbf{R} = \mathbf{R}_s + \mathbf{R}_b^2 = \frac{1}{96} \begin{bmatrix} 1 \\ 2 \\ 1 \\ 2 \end{bmatrix} + \begin{bmatrix} 0 \\ 3 \\ 3 \\ 0 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 1 \\ 290 \\ 289 \\ 2 \end{bmatrix}.$$

Osnovni rubni uvjeti

$$T_3 = 8, T_4 = 5.$$

$$\frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & -1 \\ -1 & 2 & -1 & 0 \\ 0 & -1 & 2 & -1 \\ -1 & 0 & -1 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2 \\ 290 \\ 289 \\ 1 \end{bmatrix},$$

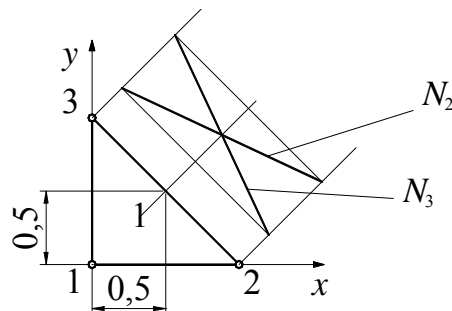
$$\frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & -1 \\ -1 & 2 & 0 & 0 \\ 0 & 0 & 2 & 0 \\ -1 & 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2 \\ 290 \\ 289 \\ 1 \end{bmatrix} - 8 \frac{1}{2} \begin{bmatrix} 0 \\ -1 \\ 2 \\ -1 \end{bmatrix},$$

$$\frac{1}{2} \begin{bmatrix} 2 & -1 & 0 & 0 \\ -1 & 2 & 0 & 0 \\ 0 & 0 & 2 & 0 \\ 0 & 0 & 0 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2 \\ 290 \\ 289 \\ 1 \end{bmatrix} - 8 \frac{1}{2} \begin{bmatrix} 0 \\ -1 \\ 2 \\ -1 \end{bmatrix} - 5 \frac{1}{2} \begin{bmatrix} -1 \\ 0 \\ 0 \\ 2 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 2+240 \\ 290+384 \\ 768 \\ 480 \end{bmatrix}.$$

$$\frac{1}{2} \begin{bmatrix} 2 & -1 \\ -1 & 2 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \end{bmatrix} = \frac{1}{96} \begin{bmatrix} 242 \\ 674 \end{bmatrix}.$$

$$\begin{bmatrix} T_1 \\ T_2 \end{bmatrix} = \begin{bmatrix} 8,0347 \\ 11,0278 \end{bmatrix}.$$

Točka u sredini ploče ima koordinate $(x, y) = (0,5, 0,5)$, tj. nalazi se na stranici koja spaja čvorove 2 i 4 proračunskog modela. Uzeto Budući da je za KE1 na toj stranici funkcija oblika N_1 jednaka nuli, a za KE2 na toj stranici funkcija oblika N_2 i na osnovi tablice podudaranja lokalnih i globalnih čvornih varijabli, može se uzeti za KE1 raspodjela funkcije nezavisne varijable pa stranici koja spaja globalne čvorove 2 i 4. Slijedi



$$\phi(0,5, 0,5) = N_2(0,5, 0,5)\phi_2^1 + N_3(0,5, 0,5)\phi_3^1.$$

$$\phi(0,5, 0,5) = \frac{1}{2} 11,0287 + \frac{1}{2} 5 = 8,014.$$